

2nd AIAA Sonic Boom Prediction Workshop

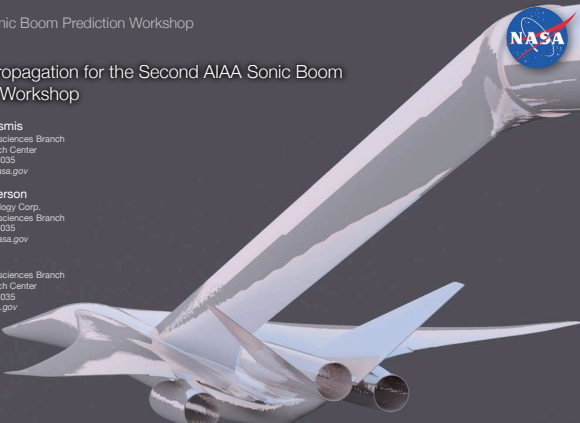
sBOOM Propagation for the Second AIAA Sonic Boom Prediction Workshop

Michael J. Aftosmis
Computational Aerospaces Branch
NASA Ames Research Center
Moffett Field, CA 94035
michael.aftosmis@nasa.gov

George R. Anderson
Science and Technology Corp.
Computational Aerospaces Branch
NASA Ames Research Center
Moffett Field, CA 94035
george.anderson@nasa.gov

Marian Nemec
Computational Aerospaces Branch
NASA Ames Research Center
Moffett Field, CA 94035
marian.nemec@nasa.gov

7-8 Jan 2017, Grapevine TX, USA



Outline

- Intro - codes, conventions and studies
 - Wind Convention
 - Mesh refinement
 - Accuracy requirements
- "Axibody" - Body of revolution
- "LM 1021" - Wind tunnel model of full configuration from 2014 boom workshop
- Summary

2

Introduction

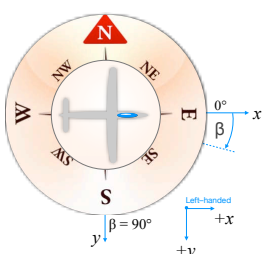
- Propagation using sBOOM (v2.5)* for all cases
 - Augmented Burgers' eq.
 - Finite-difference with space-operator splitting
 - Most runs under 1 min on laptop
- Loudness metrics computed with LCASB†
- Applied current "best practices"
- Mesh refinement study done for both geometries using std. atm.
- Ran all required & optional cases

* Rallabhandi, S. "Advanced Sonic Boom Prediction Using the Augmented Burgers Equation"
J. of Aircraft 48:1245-1253, 2011.

† Shepard & Sullivan, "Loudness Code for Asymmetric Sonic Booms (LCASB)", NASA TP 3134, 1991

3

Wind Convention



- sBOOM uses left-handed coordinate system for wind
- β = heading,
 - $\beta = 0^\circ$ A/C pointed East
 - Clockwise = $+\beta$
- sBOOM wind tables are in meters vs m/s
- x and y inputs are wind components ("blows toward")
 - $(x, y) = (1, 0)$ is tail wind if heading is East
 - $(x, y) = (0, 1)$ is tail wind if heading is South
 - $(x, y) = (1, 1)$ is tail wind if heading is South-East

Net result is that sign on y-component of wind in the workshop wind-specification needs to be flipped. $(W_x, W_y)_{\text{sBOOM}} = (W_x, -W_y)_{\text{workshop}}$

4

Mesh Convergence

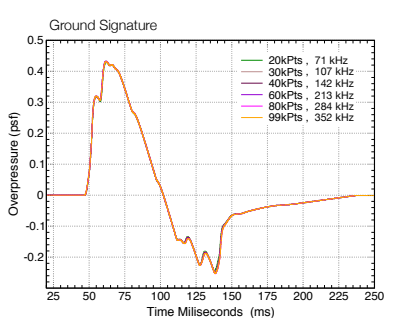
Sensitivity of noise output to mesh refinement

- Propagation code is solving augmented Burgers' via finite difference
- Need to make sure we're getting mesh converged result
- Mesh convergence is case dependent
 - Do for each case, assume std atmosphere
- Dissipation due to truncation error directly impacts accuracy, resolution requirements are driven by need to minimize error in propagation
 - Initial signal typically has < 2 k pts
 - Propagation typically requires 20-50 kpts

5

Mesh Convergence

Sensitivity of noise output to refinement of the propagation mesh

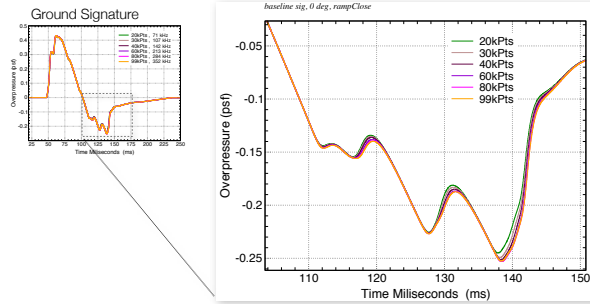


6



Mesh Convergence

Sensitivity of noise output to refinement of the propagation mesh

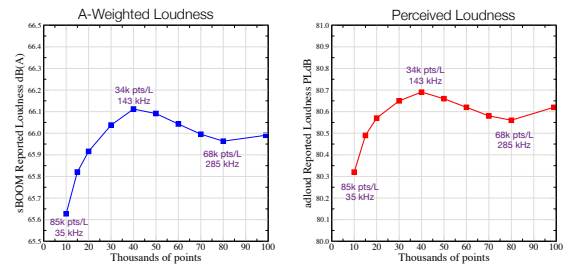


7



Mesh Convergence

Sensitivity of noise output to refinement of the propagation mesh



- Both dB(A) and PLdB show similar behavior
- Lower than 35 kHz, noise outputs drops quickly
- However, mesh convergence not convincing, even at higher frequencies

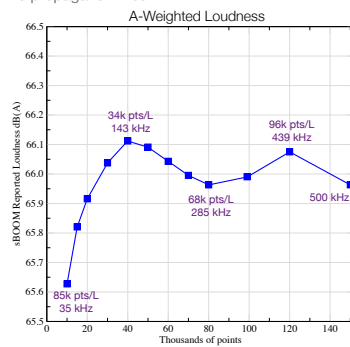
8



Mesh Convergence

Sensitivity of noise output to refinement of the propagation mesh

- Ran up to 500 kHz
- Mesh convergence still not convincing
- At 500 kHz, oversampling original signal by nearly 100:1
- Possibility of aliasing due to oversampling



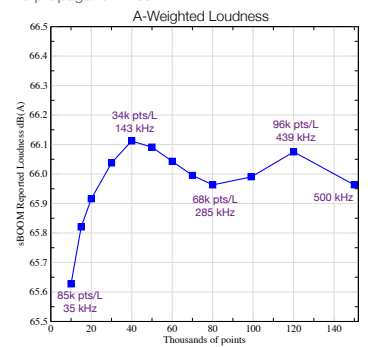
9



Mesh Convergence

Sensitivity of noise output to refinement of the propagation mesh

- Slow mesh convergence not surprising
- Signal is non-smooth, and integrated loudness outputs are very sensitive
- Oversampling introduces higher frequencies which may effect loudness output

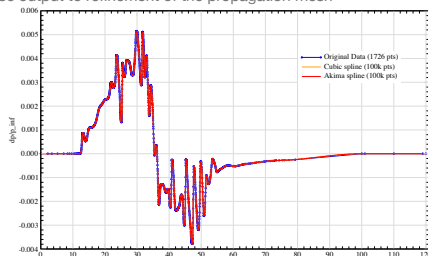


10



Mesh Convergence

Sensitivity of noise output to refinement of the propagation mesh



- Spline data at high resolution with Akima spline
- Pass high-resolution data from splined signal into sBOOM to avoid aliasing high-frequencies

11

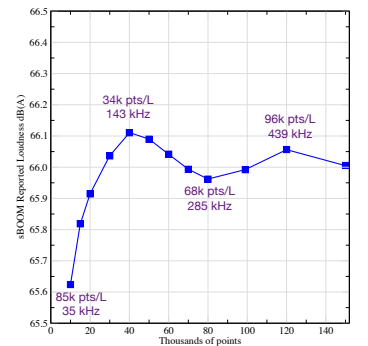


Mesh Convergence

Spline data to avoid aliasing

- Somewhat better mesh behavior at high frequencies, but...
- Mesh convergence still not really convincing
- Need to investigate more

- Used un-splined data sampled at 107 kHz (30 kpts) for runs

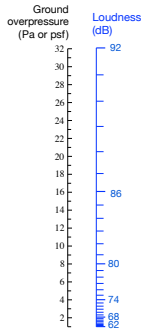


12



Caveats on Accuracy Requirements

Decibels are logarithmic units!



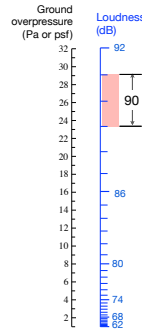
Double the loudness → ~10 dB more sensed loudness level (psycho acoustic)
Double the sound pressure level → 6 dB more measured sound pressure level

13



Caveats on Accuracy Requirements

Decibels are logarithmic units!



Double the loudness → ~10 dB more sensed loudness level (psycho acoustic)
Double the sound pressure level → 6 dB more measured sound pressure level

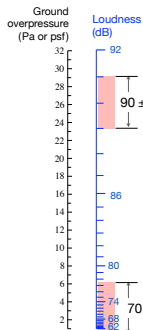
- We propagate pressure signals to the ground
→ Propagation error has units of pressure
- e.g.
 - If error of ± 2 Pa on a 90 dB signal is less than ± 1 dB
 - The same error on a 70 dB signal may be ± 6 dB
- Propagation accuracy requirements increase logarithmically as signals get quieter!
- Sampling frequency for a 90 dB signal is likely to be insufficient for a 70 dB signal

14



Caveats on Accuracy Requirements

Decibels are logarithmic units!



Double the loudness → ~10 dB more sensed loudness level (psycho acoustic)
Double the sound pressure level → 6 dB more measured sound pressure level

- We propagate pressure signals to the ground
→ Propagation error has units of pressure
- e.g.
 - If error of ± 2 Pa on a 90 dB signal is less than ± 1 dB
 - The same error on a 70 dB signal may be ± 6 dB
- Propagation accuracy requirements increase logarithmically as signals get quieter!
- Sampling frequency for a 90 dB signal is likely to be insufficient for a 70 dB signal

15



Axibody

Shaped axisymmetric body of revolution

Conditions:

$M_\infty = 1.6$
Altitude = 15849.6 m (52 kft)
 $L_{ref} = 42.98$ m (141 ft)
 $r/L = 3.0$ at signal extraction
Ground reflection factor = 1.9
Heading East ($\beta = 0^\circ$)

Cases:

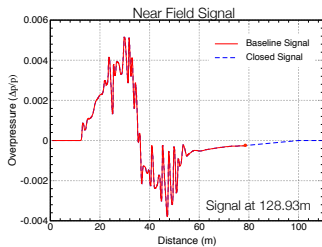
Required: Atm #3
Optional #1: Std. Atm.
Optional #2: Atm #4
Optional #4: Std. Atm. with
70% humidity

16



Axibody

Close near field signal



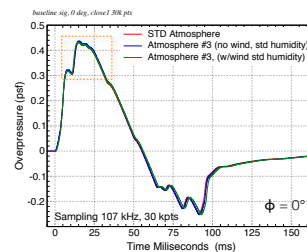
- Compared 2 different closures (both linear ramps) gave consistent results
- Closed signal using linear ramp to 0 at 100 m
- Ground signals & noise both virtually identical

17



Axibody

Ground signature – Atmosphere #3 vs Standard Atmosphere



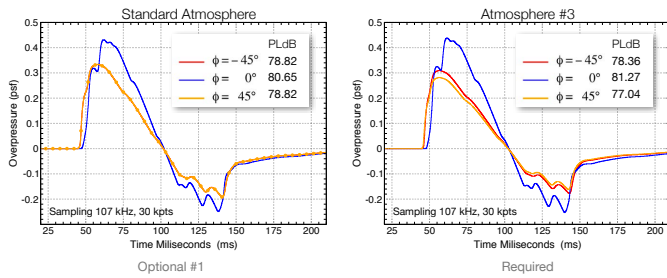
- Atmosphere 3 was required case
- ~0.6 PLdB louder than standard atmosphere

18



Axibody

Ground signature – Standard Atm. vs Atmosphere 3, $\phi = \{-45^\circ, 0^\circ, 45^\circ\}$

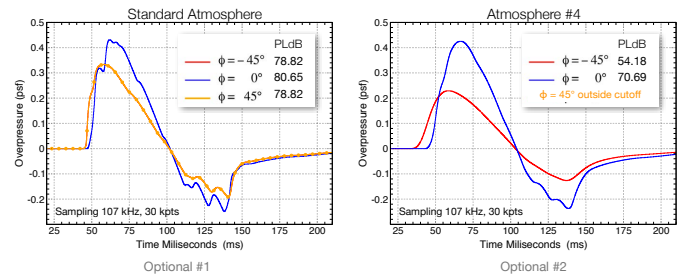


19



Axibody

Ground signature – Standard Atm. vs Atmosphere 4, $\phi = \{-45^\circ, 0^\circ, 45^\circ\}$

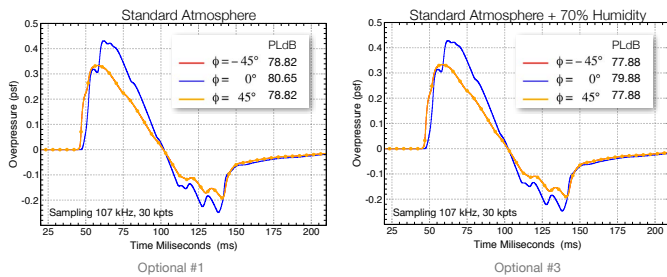


20



Axibody

Ground signature – Standard Atm. vs Standard Atm. + 70% Relative Humidity

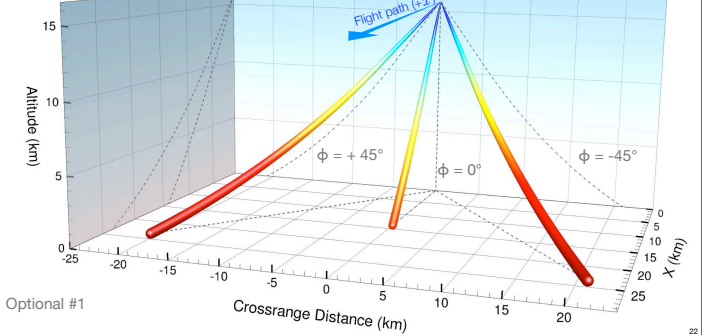


21



Axibody

Raytubes, standard atmosphere

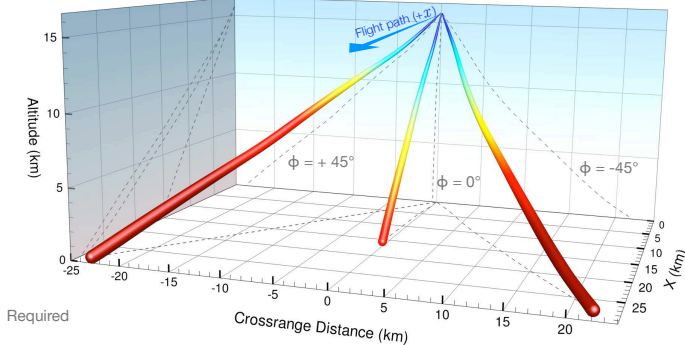


22



Axibody

Raytubes, Atm #3

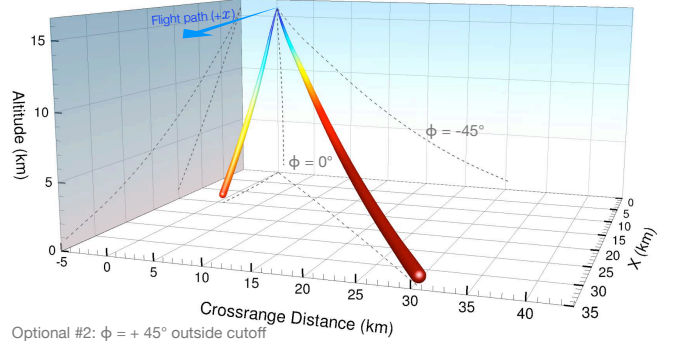


33

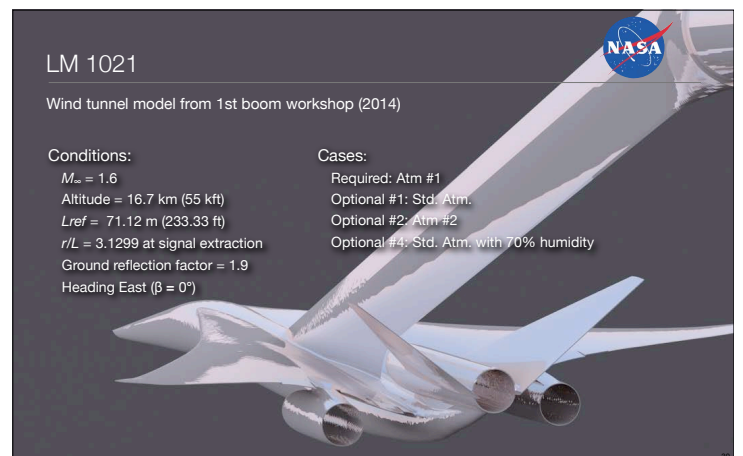
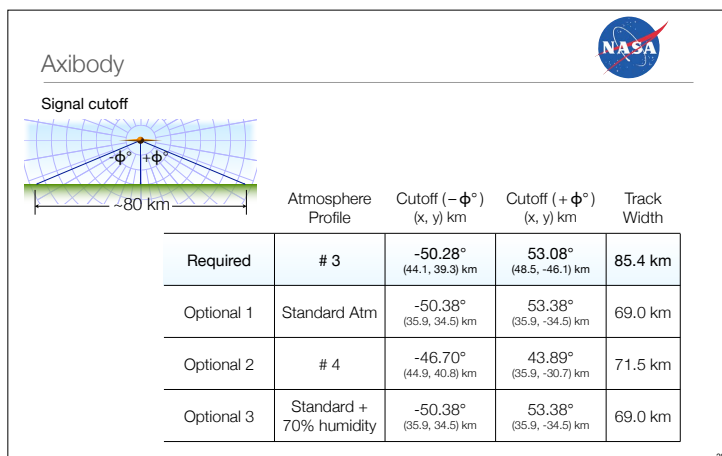
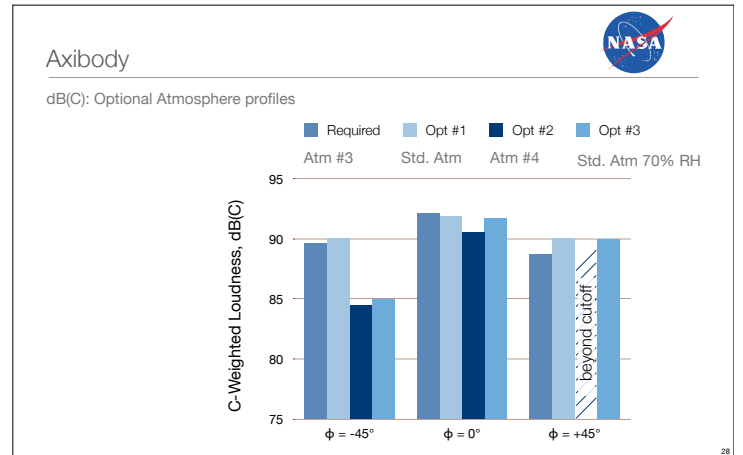
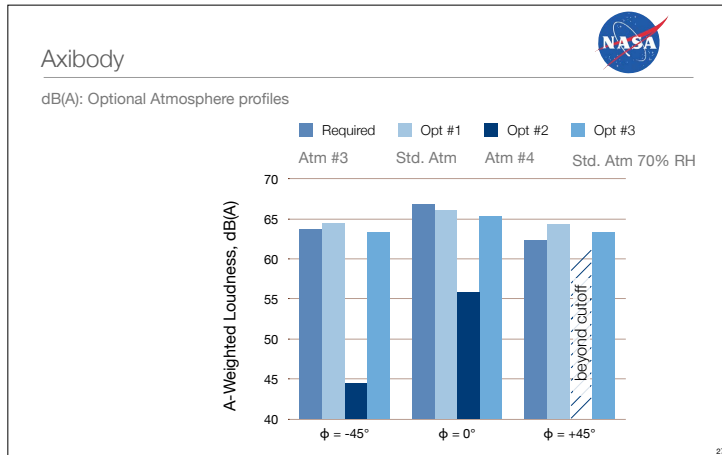
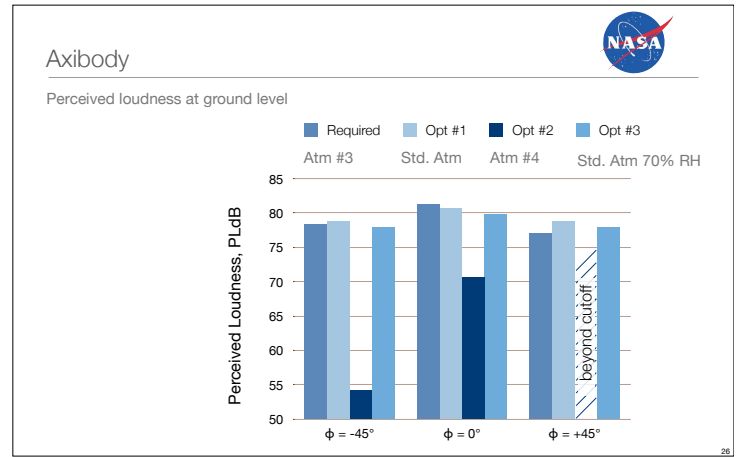
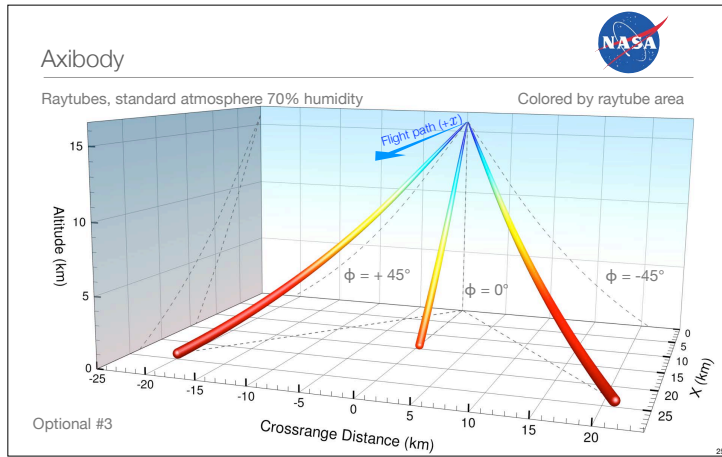


Axibody

Raytubes, atmosphere 4



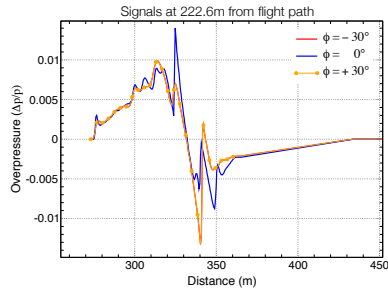
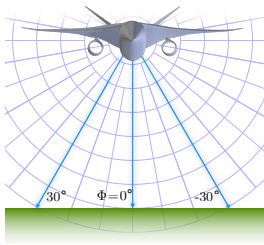
24





LM 1021

Near Field Signatures



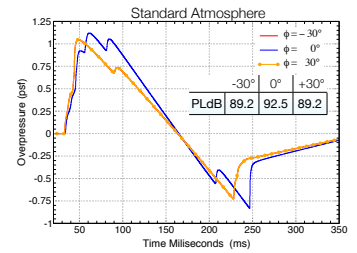
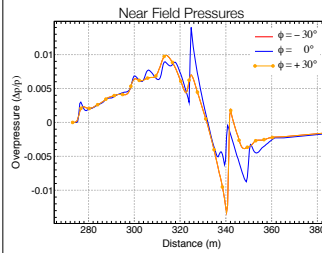
Signals closed with a linear ramp to 435 m

31



LM 1021

Ground signature: Standard Atmosphere, $\phi = \{-30^\circ, 0^\circ, 30^\circ\}$



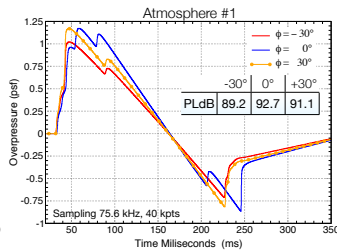
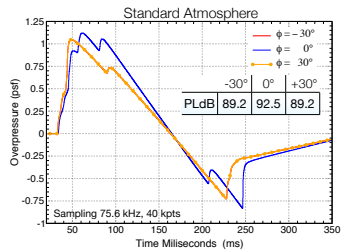
Sampling Frequency = 75.6 kHz, 40 kpts

32



LM 1021

Ground signature – Atmosphere #1, $\phi = \{-30^\circ, 0^\circ, 30^\circ\}$

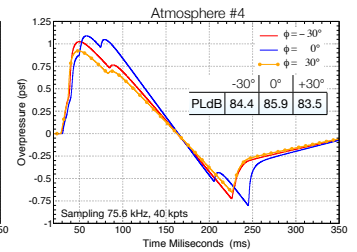
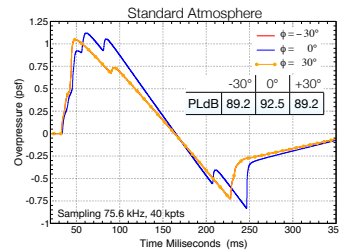


33



LM 1021

Ground signature – Optional #2, Atmosphere #4, $\phi = \{-30^\circ, 0^\circ, 30^\circ\}$



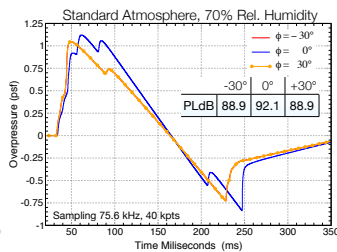
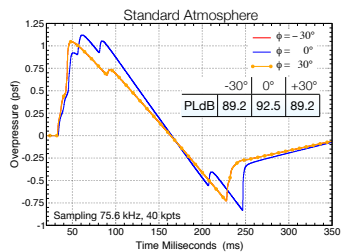
~5 dB quieter than Std. Atm. conditions

34



LM 1021

Ground signature – Optional #3, std/ atm. +70% relative humidity, $\phi = \{-30^\circ, 0^\circ, 30^\circ\}$



Slightly quieter (0.3-0.4 dB) than in std atmosphere

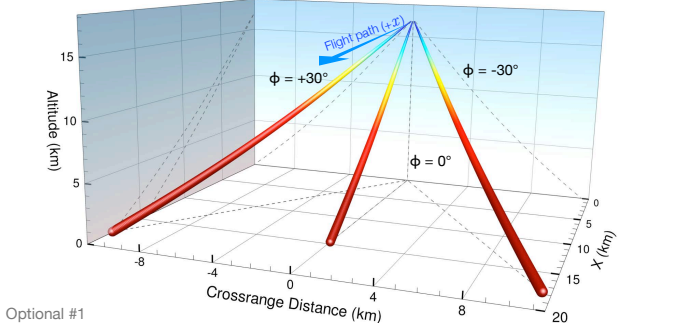
35



LM 1021

Raytubes, Standard Atmosphere

Colored by raytube area



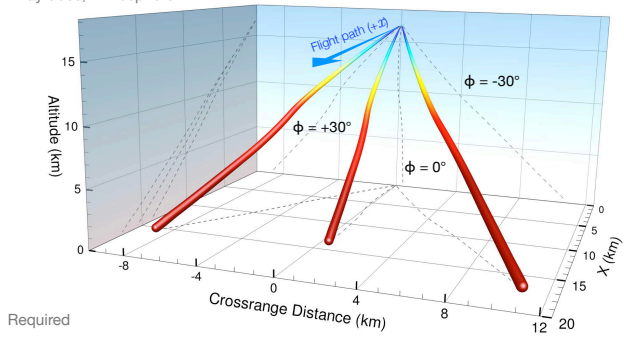
Optional #1

36



LM 1021

Raytubes, Atmosphere #1



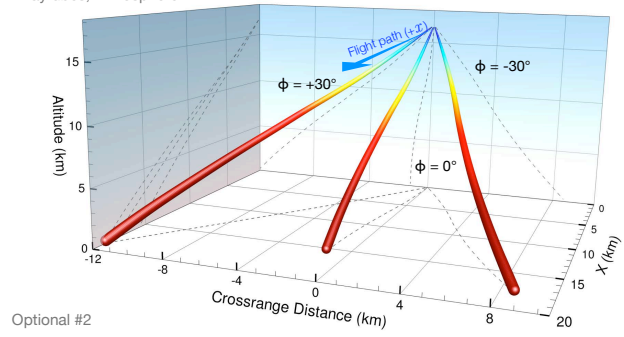
Required

37



LM 1021

Raytubes, Atmosphere #2



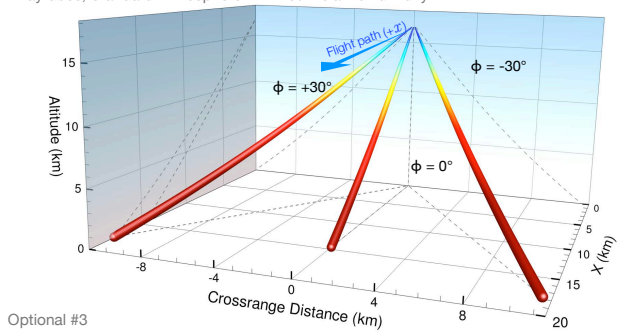
Optional #2

38



LM 1021

Raytubes, Standard Atmosphere with 70% relative humidity



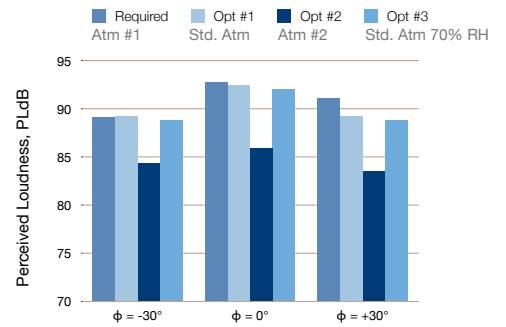
Optional #3

39



LM 1021

Perceived loudness at ground level

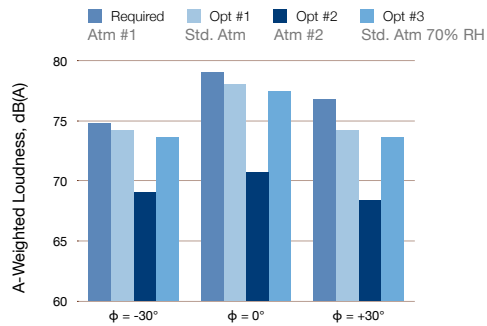


40



LM 1021

A-Weighted Loudness at ground level

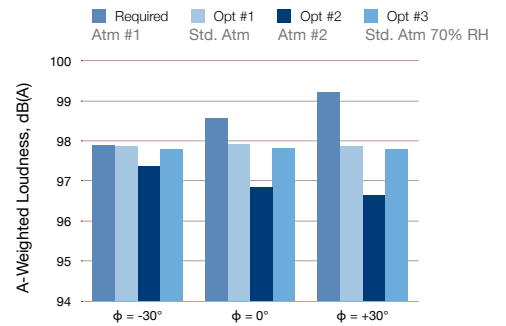


41



LM 1021

A-Weighted Loudness at ground level

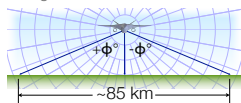


42



LM 1021

Signal cutoff



	Atmosphere Profile	Cutoff ($-\phi^\circ$) (x, y) km	Cutoff ($+\phi^\circ$) (x, y) km	Track Width
Required	# 1	-57° (40.0, 42.3) km	74° (39.4, -44.6) km	86.9 km
Optional 1	Standard Atm	-50.38° (37.0, 35.6) km	50.38° (37.0, -35.6) km	71.2 km
Optional 2	# 2	-64.65° (43.9, 41.7) km	59.35° (67.0, -69.7) km	111.4 km
Optional 3	Standard + 70% humidity	-50.38° (37.0, 35.6) km	50.38° (37.0, -35.6) km	71.2 km

43



Summary

- Applied sBOOM and LCASB for all required and optional cases
- Showed difficulty in obtaining mesh-converged loudness metrics
 - Noted issues due to oversampling
 - Noted that resolution requirements increase as signals get quieter
- Open questions & Opportunities
 - Impact of step-size on mesh convergence?
 - Splining of the input
 - Consider higher-order discretization to control truncation error at lower sampling rates
 - Automatic output-based adaptation of sBOOM propagation mesh for loudness functional

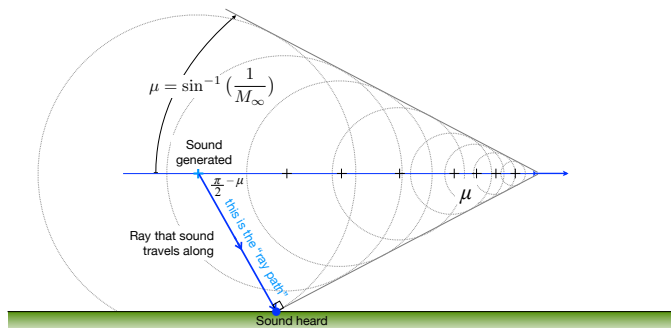
44

Questions?



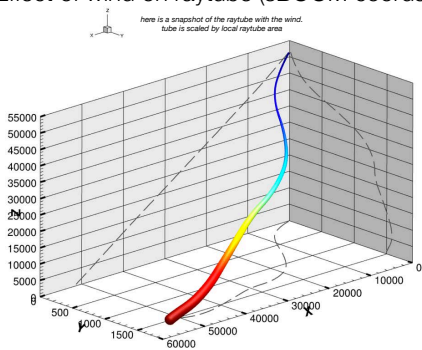
understanding the ray path

2017.08.11



Effect of wind on raytube (sBOOM coords)

2017.08.27



• "% sBOOM 2.5 -v -d" reports:
Ground intercept for Azimuth: 0.000000
- Propagation time: 68.010707 (s)
- X = 51811.993216 (ft) Y = 1478.793091 (ft)